Mathematical Exploration of New Ideas Surrounding Capillarity Understanding in Science (M.E.N.I.S.C.U.S.)

Matthew Kearney, Laura Nicholson, Zachary Richey

George Mason University, MEGL

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- Capillary Action: Dynamics of Fluid Rise and Porous Media
- Literature: Mixture Theory, Lago & Araujo, Brooks & Corey
- Quasi-Steady Model: Theory, Algorithm, and Results
- Unsteady Flow
- Ideas Moving Forward

What is Capillary Action?

- Fluid molecules stick to their container and to each other.
- This creates surface tension.
- Fluid rises through its container.
- Can happen in a **tube** or a **porous material**.





Capillary Dynamics

Navier-Stokes Equations (circa 1821)

$$\rho \left(\frac{\partial \vec{u}}{\partial t} + \vec{u} \cdot \nabla \vec{u} \right) = -\nabla P + \mu \nabla^2 \vec{u} + \rho \vec{g}$$
$$\nabla \cdot \vec{u} = 0$$

- We can add extra restrictions and boundary conditions to model capillary action in a tube.
- Let *h* be the **capillary height**.

Washburn Equation (1921)

$$h(t) = \sqrt{Dt}$$
, where $D := \frac{\gamma r \cos \theta}{2\mu}$

Porous Materials





Figure: A partially saturated sponge.

- treats a point in the porous media as a small volume containing some proportion of solid, liquid, and gas.
- define fluid velocity and pressure at each point

Saturation of Porous Media
$$\phi_\ell + \phi_s + \phi_g = 1$$
 $S := rac{\phi_\ell}{1 - \phi_s}$

Brooks & Corey (1964): Background

- investigation of drainage and irrigation models
- Earlier models neglected partial saturation and air/water pressure differential
- assumes flow of immiscible gas/liquid phases within continuous porous network



- Materials studied: Volcanic Sand, Fine Sand, Glass Beads, Silt Loam, Sandstone, and Clay/Sandstone/Sand mixture
- Figure: Capillary Pressure versus Saturation. Note asymptotic behavior as $S \rightarrow S_r$

Brooks & Corey (1964): Models

Capillary Pressure

$$p_c(S) = p_c^0 \left(\frac{1-S_r}{S-S_r}\right)^{1/2}$$

Relative Permeability (Burdine Equations)

$$k_{r\ell}(S) = \left(\frac{S-S_r}{1-S_r}\right)^{3+2/2}$$

• S := saturation

- S_r := residual saturation constant
- $\lambda :=$ pore size distribution index

Mixture Theory

- Assume only vertical flow
- Mass Balance:

$$\frac{\partial \phi_\ell}{\partial t} = -\frac{\partial}{\partial z} (w_\ell \phi_\ell)$$

• Momentum Balance (Darcy's Law):

$$\frac{\partial p_c}{\partial z} = \frac{K_{s\ell}}{\phi_\ell} w_\ell + \Delta \rho g$$

Hence:

$$w_{\ell} = \frac{\phi_{\ell}}{K_{s\ell}} \left(\frac{\partial p_{c}}{\partial z} - \Delta \rho g \right)$$

$$\frac{\partial \phi_{\ell}}{\partial t} = -\frac{\partial}{\partial z} \left[\frac{\phi_{\ell}^2}{K_{s\ell}} \left(\frac{\partial p_c}{\partial z} - \Delta \rho g \right) \right]$$



Figure: A partially saturated sponge.

- w_{ℓ} : liquid velocity
- $\Delta \rho = \rho_{\ell} \rho_{g}$: density difference
- $p_c = p_\ell p_g$: capillary pressure
- $K_{s\ell}$: friction coefficient ($\propto k_{r\ell}^{-1}$)

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Let *h*_ℓ be the **height** of the liquid fraction:

$$\frac{dh_\ell}{dt} = w_\ell(z = h_\ell)$$

$$\frac{dh_{\ell}}{dt} = \left. \frac{\phi_{\ell}}{K_{s\ell}} \left(\frac{\partial p_c}{\partial z} - \Delta \rho g \right) \right|_{z=h_{\ell}}$$

• Boundary Conditions:

$$\phi_\ell(z=0) := \phi_\ell^0$$

 $\phi_\ell(z=h_\ell) := \phi_\ell^1$



Figure: A partially saturated sponge.

- w_{ℓ} : liquid velocity
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Nondimensionalization

Let's nondimensionalize this:

$$z = \left(rac{p_c(\phi_\ell^0)}{\Delta
ho g}
ight) ar{z}, \qquad t = rac{\mu}{k_0 p_c(\phi_\ell^0)} \left(rac{p_c(\phi_\ell^0)}{\Delta
ho g}
ight)^2 ar{t},$$

$$h_{\ell}(t) = \left(rac{p_c(\phi_{\ell}^0)}{\Delta
ho g}
ight) ar{h}_{\ell}(t), \quad p_c(\phi_{\ell}) = \left(rac{1}{p_c(\phi_{\ell}^0)}
ight) ar{p}_c(\phi_{\ell})$$

 \implies

Dimensional Forms

Dimensionless Forms

$$\frac{\partial \phi_{\ell}}{\partial t} = -\frac{\partial}{\partial z} \left[\frac{\phi_{\ell}^2}{K_{s\ell}} \left(\frac{\partial p_c}{\partial z} - \Delta \rho g \right) \right] \Longrightarrow \frac{\partial \phi_{\ell}}{\partial \bar{t}} = \frac{\partial}{\partial \bar{z}} \left[k_{r\ell}(\phi_{\ell}) \left(-\frac{\partial \bar{p}_c}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right) \right]$$
$$\frac{dh_{\ell}}{dh_{\ell}} = \frac{\phi_{\ell}}{k_{r\ell}} \left(\frac{\partial p_c}{\partial \bar{z}} - \Delta \rho g \right) = \frac{d\bar{h}_{\ell}}{k_{r\ell}} \left(\frac{\partial \bar{p}_c}{\partial \bar{z}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right) = \frac{d\bar{h}_{\ell}}{k_{r\ell}} \left(\frac{\partial p_c}{\partial \bar{z}} - \Delta \rho g \right)$$

$$\frac{dn_{\ell}}{dt} = \frac{\phi_{\ell}}{K_{s\ell}} \left(\frac{\partial p_c}{\partial z} - \Delta \rho g \right) \Big|_{z=h_{\ell}} \Longrightarrow \frac{dn_{\ell}}{d\overline{t}} = -\frac{\kappa_{r\ell}(\phi_{\ell})}{\phi_{\ell}} \left(-\frac{\partial p_c}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \overline{z}} + 1 \right) \Big|_{\overline{z}=\overline{h}_{\ell}}$$

Quasi-steady Flow

• Goal: Solve for $\bar{h}_\ell(t)$

$$\frac{\partial \phi_{\ell}}{\partial \bar{t}} = \frac{\partial}{\partial \bar{z}} \left[k_{r\ell}(\phi_{\ell}) \left(-\frac{\partial \bar{p}_c}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right) \right]$$

$$rac{dar{h}_\ell}{dar{t}} = -rac{k_{r\ell}(\phi_\ell)}{\phi_\ell} \left(-rac{\partialar{p}_c}{\partial\phi_\ell}rac{\partial\phi_\ell}{\partialar{z}} + 1
ight) igg|_{ar{z}=ar{h}_\ell}$$

• Assume flow is **quasi-steady**, i.e. $\frac{\partial \phi_{\ell}}{\partial \bar{t}} = 0$

$$0 = \frac{\partial}{\partial \bar{z}} \left[k_{r\ell}(\phi_{\ell}) \left(-\frac{\partial \bar{p}_{c}}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right) \right]$$
$$C(\bar{t}) = k_{r\ell}(\phi_{\ell}) \left(-\frac{\partial \bar{p}_{c}}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right)$$
$$\frac{d \bar{h}_{\ell}}{d \bar{t}} = -\frac{C(\bar{t})}{\phi_{\ell}} \Big|_{\bar{z} = \bar{h}_{\ell}} = -\frac{C(\bar{t})}{\phi_{\ell}^{1}}$$

Brooks & Corey Model

According to Brooks & Corey:

$$p_{c}(S(\phi_{\ell})) = p_{c}^{0} \left(rac{1-\phi_{s}}{1-S_{r}} \phi_{\ell} + rac{-S_{r}}{1-S_{r}}
ight)^{-1/\lambda} =:$$
 Capillary Pressure

$$k_{r\ell}(S(\phi_\ell)) = \left(rac{1-\phi_s}{1-S_r}\phi_\ell + rac{-S_r}{1-S_r}
ight)^{3+2/\lambda} =:$$
 Relative Permeability

$$-\frac{\partial \bar{p}_{c}}{\partial \phi_{\ell}} = \alpha \gamma (\alpha \phi_{\ell} + \beta)^{-1-\gamma}$$

$$k_{r\ell}(\phi_{\ell}) = (\alpha \phi_{\ell} + \beta)^{3+2\gamma}$$

Integration

• Plug these functions into our equation:

$$C(\bar{t}) = k_{r\ell}(\phi_{\ell}) \left(-\frac{\partial \bar{p}_{c}}{\partial \phi_{\ell}} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + 1 \right)$$

$$C(\bar{t}) = \alpha \gamma (\alpha \phi_{\ell} + \beta)^{2+\gamma} \frac{\partial \phi_{\ell}}{\partial \bar{z}} + (\alpha \phi_{\ell} + \beta)^{3+2\gamma}$$

• Separation of variables:

$$d\bar{z} = \frac{\alpha\gamma(\alpha\phi_{\ell}+\beta)^{2+\gamma}}{C(\bar{t}) - (\alpha\phi_{\ell}+\beta)^{3+2\gamma}} d\phi_{\ell}$$

$$h_{\ell}(\bar{t}) = \int_{\phi_{\ell}^{0}}^{\phi_{\ell}^{1}} \frac{\alpha \gamma (\alpha \phi_{\ell} + \beta)^{2+\gamma}}{C(\bar{t}) - (\alpha \phi_{\ell} + \beta)^{3+2\gamma}} d\phi_{\ell}$$

Numerical Simulation

$$\frac{d\bar{h}_{\ell}}{d\bar{t}} = -\frac{C(\bar{t})}{\phi_{\ell}^{1}}$$
(1)
$$h_{\ell}(\bar{t}) = \int_{\phi_{\ell}^{0}}^{\phi_{\ell}^{1}} \frac{\alpha\gamma(\alpha\phi_{\ell}+\beta)^{2+\gamma}}{C(\bar{t}) - (\alpha\phi_{\ell}+\beta)^{3+2\gamma}} d\phi_{\ell}$$
(2)
$$\phi_{\ell}(\bar{z}=0) := \phi_{\ell}^{0}, \quad \phi_{\ell}(\bar{z}=\bar{h}_{\ell}) := \phi_{\ell}^{1}$$

- Let $F(\bar{h}_{\ell}) = C$ be the function given implicitly by (2)
- Numerical approach:

$$\begin{split} \bar{t} \leftarrow \bar{t}_0; \quad \bar{h}_\ell(0) \leftarrow \bar{h}_\ell^0; \quad C(0) \leftarrow C_0 \\ \text{While } \bar{t} < \bar{t}_{max}: \\ \bar{h}_\ell \leftarrow \bar{h}_\ell - (C/\phi_1) d\bar{t} \\ C \leftarrow F(\bar{h}_\ell) \\ \bar{t} \leftarrow \bar{t} + d\bar{t} \end{split}$$

Zero Gravity

Suppose gravity is negligible, i.e. g = 0:

Integrate:
$$h_{\ell}(\bar{t}) = \int_{\phi_{\ell}^{0}}^{\phi_{\ell}^{1}} \frac{\alpha \gamma (\alpha \phi_{\ell} + \beta)^{2+\gamma}}{C(\bar{t}) - (\alpha \phi_{\ell} + \beta)^{3+2\gamma}} d\phi_{\ell}$$

Substitute (1):
$$C(\bar{t}) = rac{\gamma(\alpha\phi_\ell^1 + \beta)^{3+\gamma} - \gamma(\alpha\phi_\ell^0 + \beta)^{3+\gamma}}{(3+\gamma)\bar{h}_\ell(\bar{t})}$$

Solve ODE:
$$\frac{d\bar{h}_{\ell}}{d\bar{t}} = -\frac{C(\bar{t})}{\phi_{\ell}^{1}} = \frac{\gamma(\alpha\phi_{\ell}^{0}+\beta)^{3+\gamma}-\gamma(\alpha\phi_{\ell}^{1}+\beta)^{3+\gamma}}{\phi_{\ell}^{1}(3+\gamma)\bar{h}_{\ell}(\bar{t})}$$

$$\bar{h}_{\ell}(\bar{t}) = \sqrt{\bar{t}\left(\frac{\gamma(\alpha\phi_{\ell}^{0} + \beta)^{3+\gamma} - \gamma(\alpha\phi_{\ell}^{1} + \beta)^{3+\gamma}}{\phi_{\ell}^{1}(3+\gamma)}\right)}$$

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Equilibrium height

$$\frac{d\bar{h}_{\ell}}{d\bar{t}} = -\frac{C(\bar{t})}{\phi_{\ell}^1} = 0$$

 $C(\bar{t}) = 0$

$$h_{\ell}^{eq} = \int_{\phi_{\ell}^{0}}^{\phi_{\ell}^{1}} \frac{\alpha \gamma (\alpha \phi_{\ell} + \beta)^{2+\gamma}}{\mathcal{F}(\overline{t})^{-0} (\alpha \phi_{\ell} + \beta)^{3+2\gamma}} d\phi_{\ell}$$

$$\left| ar{h}_{\ell}^{eq} = rac{1}{(lpha \phi_{\ell}^1 + eta)^{\gamma}} - rac{1}{(lpha \phi_{\ell}^0 + eta)^{\gamma}}
ight|$$

Numerical Results



- Simulation behavior consistent with model in zero-gravity case
- Simulation equilibrium height consistent with model
- Similar shape as seen in experiments, but no clear $t^{1/2}$ or $t^{1/4}$ regimes

Numerical Simulation of Unsteady Flow

- We studied a problem involving the flow of a liquid confined between parallel walls.
- It is essentially a 2-dimensional problem, different from the 3-D problems of flow in tubes.
- Discretizing into a many distinct x-values allows us to convert the PDE into a system of many ODEs.
- zero gravity, but unsteady flow



Assume that the meniscus is approximately flat, and that capillary pressure is $% \left({{{\left({{{c}} \right)}}_{0}}_{0}} \right)$ constant

Numerical Simulation Details

- Keep assumptions related to the Washburn-type model for parallel plates, but allow velocity to change over time.
- Assume that:





Future Work

- Further exploration using numerical simulation
- Use asymptotic & perturbation methods to find an analytic solution
- Attempt to solve without relying upon quasi-steady assumption
- Incorporate material deformation





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